## INTRODUCTION TO X-RAY DIFFRACTION

## By

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## Introduction



1. X-rays were discovered by scientist W. Rontgen in 1895.
2. X-rays are high energy electro magnetic waves having very short wavelength ranging from 0.01 to 10 nm .
3. The longer wavelength (smaller energy : <10 keV) end of X-ray spectrum is known as soft X-rays and shorter wavelength end (higher energy : $>10 \mathrm{keV}$ ) is known as hard x-rays.
4. In 1912, diffraction pattern of X-rays was first obtained by Max Laue.

## Applications of X rays

- X-ray photographs are used to detect bone fracture or presence of foreign object in a human body.
- They are used to cure skin diseases and to destroy tumors.
- They are used to detect flaws and cracks in metallic parts of cars, aeroplanes etc.
- They are used to study crystal structures.


## Properties of X-rays

- X-rays travel in a straight line.
- Can not be deflected by electric or magnetic field.
- X-rays have high penetrating power.
- Fluorescent materials glow when X-rays are directed at them.
- Photoelectric emission can be produced by X-rays and also used for elemental composition (XPS, EDAX).
- Ionizes gas molecule when an X-ray beam is passed through gas container.
- X-rays are diffracted by crystals.


## Production of X-rays



Figure: Schematic diagram of Coolidge X-ray tube

1. Target element should have high melting point and high atomic number.
2. Intensity of $X$-rays depends upon temperature of filament
3. Frequency (i.e. Energy) of X-rays depends upon P.D. between cathode and anode

## The Principle of generation of continuous spectrum



1. Continuous spectrum arises due to the deceleration of the electrons hitting the target
2. This type of radiation is known as bremsstrahlung, German word for "braking radiation"
3. It is also called polychromatic, continuous or white radiation

## Continuous Spectrum



The Principle of generation of characteristic spectrum


L-shell to K-shell jump produces a $K_{\alpha}$ x-ray
M-shell to K-shell jump produces a $K_{\beta}$ x-ray

1. An incoming high-energy electron
dislodges a k-shell electron in the
target, leaving a vacancy in the K
shell
2. An outer shell electron then "jumps"
to fill the vacancy
3. A characteristic x-ray (equivalent to
the energy change in the "jump") is
generated


X-ray spectrum of Mo at different voltage

1. Characteristic spectra is also called as line spectra of target element
2. The spectrum remains all "white" without any peaks till the potential difference reaches a certain higher limit. Above certain potential difference line spectra is observed.
3. Characteristic spectra or line spectra is characteristic of target element.

## Some Commonly Used characteristic X-ray K wavelengths (Å)

|  |  |  | Element | K $\alpha$ (av.) | K $\alpha_{1}$ | K $\alpha_{2}$ | K $\beta_{1}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: | :---: |
|  |  |  | Cr | 2.29100 | 2.28970 | 2.29361 | 2.08487 |
| $K \alpha$ | ${ }^{\kappa \alpha}$ |  | Fe | 1.93736 | 1.93604 | 1.93998 | 1.75661 |
|  |  |  | Co | 1.79026 | 1.78897 | 1.79285 | 1.62079 |
|  |  |  | Cu | 1.54184 | 1.54056 | 1.54439 | 1.39222 |
|  |  |  | Mo | 0.71073 | 0.70930 | 0.71359 | 0.63229 |

1. Usually only the K -lines are useful in x -ray diffraction
2. There are several lines in the $K$-set. The strongest are $K \alpha_{1}, K \alpha_{2}, K \beta_{1}$
3. $\alpha_{1}$ and $\alpha_{2}$ components are not always resolved $K \alpha$ doublet. $K \alpha_{1}$ is always about twice as strong as $K \alpha_{2}$, while ratio of $K \alpha_{1}$ to $K \beta_{1}$ averages about 5/1.

## Use of filter for filtering $\mathrm{CuK}_{\beta}$ radiation



Characteristic x-ray spectrum of Cu a) without any filter and b) using Ni filter

# X-ray Diffraction 

## Why X-rays are used for diffraction?

- For diffraction of a wave, the size of obstacle or aperture should be comparable to wavelength of wave.
- For electromagnetic radiation to be diffracted the spacing in the grating should be of the same order as the wavelength of radiation.
- In crystals the typical interatomic spacing is of the order of $1 \AA$ so the suitable radiations for diffraction are X -rays, because their wavelengths lies in 0.1 Å to 100 Å range.
- Hence, X-rays can be used for the study of crystal structures.


## Selection of Anode Material according to different application

| Anode <br> Material | Atomic <br> Number | Application |
| :--- | :--- | :--- |
| Copper (Cu) | 29 | Suitable for most diffraction examinations - most widely used <br> anode material. |
| Molybdenum <br> (Mo) | 42 | Preferably used for examinations on steels and metal alloys <br> with elements in the range Titanium (Ti) (atomic No. = 22) <br> to approx. Zinc (Zn) (atomic No. = 30) |
| Cobalt (Co) | 27 | Often used with ferrous samples, the Iron (Fe) fluorescence <br> radiation would cause interference and cannot be eliminated <br> by other measures. |
| Iron (Fe) | 26 | Examination of ferrous samples. Also for use with minerals <br> where Co and Cr tubes cannot be used. |
| Chromium <br> (Cr) | 24 | Used for complex organic substances and also radiographic <br> stress measurements on steels. |
| Tungsten (W) | 74 | Used where an intensive white spectrum is of more interest <br> than the characteristic. |

## Bragg's Law

$$
2 d \sin \theta=n \lambda
$$

- Constructive interference only occurs for certain $\theta$ 's correlating to a ( $h \mathrm{kl}$ ) plane, specifically when the path difference is equal to $n$ wavelengths.



## X-RAY DIFFRACTION METHODS



## THE POWDER METHOD

1. This method is useful for samples that are difficult to obtain in single crystal form.
2. Here a monochromatic X-ray beam is incident on a powdered or polycrystalline sample.
3. If a powdered specimen is used, instead of a single crystal, then there is no need to rotate the specimen, because there will always be some crystals at an orientation for which diffraction is permitted.


Schematic Diagram of powder diffraction method

## Applications of XRD

Differentiation between crystalline and amorphous materials.
Determination of the structure of crystalline materials.
Determination of the crystallite size.
Determination of the orientation of crystals.
Determination of the standard deviation.
Measurement of strain, texture coefficient etc

XRD pattern of polycrystalline and amorphous material


## Peak indexing of XRD pattern of ZnO sample



## Formulae to calculate various parameters using XRD pattern

1. The interplaner distance (d) (Hexagonal system)

$$
\frac{1}{d^{2}}=\frac{4}{3} \frac{\left(h^{2}+h k+k^{2}\right)}{a^{2}}+\frac{l^{2}}{c^{2}}
$$

2. Bragg's law :

$$
2 d \sin \theta=n \lambda
$$

3. Crystallite size using Scherrer's formula, $\quad D=\frac{0.9 \lambda}{\beta \cos \theta}$

Where,
$\beta=$ FWHM (Full width at half maximum)
D = crystallite size
$\lambda=$ wavelength of X-ray $\left(1.54056 \mathrm{~A}^{0}\right)$
4. Texture coefficient

$$
T C=\frac{I_{(h k l)} / I_{0(h k l)}}{\left(\frac{1}{N}\right)\left[\sum I_{(h k l)} / I_{0(h k l)}\right]}
$$

Where,

$$
\begin{aligned}
I_{(h k l)} & =\text { Measured intensity } \\
I_{0(h k l)} & =\text { JCPDS standard intensity } \\
\mathrm{N} & =\text { number of reflections observed in X-ray diffraction pattern. }
\end{aligned}
$$

5. Standard Deviation

$$
\sigma=\frac{\sqrt{\sum I_{(h k l)}^{2}-\left(\sum I_{(h k l)}\right)^{2} / N}}{N} \quad \text { Where, } \sigma=\text { Standard deviation }
$$

6. Nelson-Riley Function

$$
\begin{aligned}
& N R F=\frac{1}{2}\left[\frac{\cos ^{2} \theta}{\sin ^{2} \theta}+\frac{\cos ^{2} \theta}{\theta}\right] \quad \text { Where, } \\
& \text { NRF }=\text { Nelson-Riley Function } \\
& \theta=\text { Bragg's angle }
\end{aligned}
$$

## 7.Strain ( $\varepsilon$ ) :

$$
\beta=\frac{\lambda}{D \cos \theta}-\varepsilon \tan \theta
$$

$$
\beta=\frac{\lambda}{D \cos \theta}-\varepsilon \frac{\sin \theta}{\cos \theta}
$$

$$
\beta \cos \theta=\frac{\lambda}{D}-\varepsilon \sin \theta
$$

$$
\left(\frac{\beta \cos \theta}{\lambda}\right)=\frac{1}{D}-\varepsilon\left(\frac{\sin \theta}{\lambda}\right)
$$



$$
y=c-m x
$$

$$
y=m x+c
$$

| Sr. No. | $2 \theta$ (degree) | O (degree) | $\sin \theta$ | $\begin{aligned} & d_{h k \mid} \text { observed } \\ & A^{0} \end{aligned}$ | (h k I) <br> plane | 'd' standard $A^{0}$ |
| :---: | :---: | :---: | :---: | :---: | :---: | :---: |
| 1 | 31.6778 | 15.8389 | 0.2727 | 2.8222 | (100) | 2.8204 |
| 2 | 34.1601 | 17.08005 | 0.2935 | 2.6226 | (002) | 2.6062 |
| 3 | 36.1594 | 18.0797 | 0.3101 | 2.4821 | (101) | 2.4806 |
| 4 | 47.4053 | 23.70265 | 0.4017 | 1.9162 | (102) | 1.9141 |
| 5 | 56.4841 | 28.24205 | 0.4729 | 1.6278 | (110) | 1.6284 |
| 6 | 62.7602 | 31.3801 | 0.5204 | 1.4793 | (103) | 1.4793 |
| 7 | 66.0204 | 33.0102 | 0.5445 | 1.4139 | (200) | 1.4102 |
| 8 | 67.6551 | 33.82755 | 0.5564 | 1.3837 | (112) | 1.381 |
| 9 | 68.9021 | 34.45105 | 0.5654 | 1.3616 | (201) | 1.3613 |
| 10 | 72.378 | 36.189 | 0.5901 | 1.3045 | (004) | 1.3031 |
| 11 | 76.7111 | 38.35555 | 0.6202 | 1.2413 | (202) | 1.2403 |

```
Name and formula
Reference code: 01-079-0207
ICSD name: Zinc Oxide
Empirical formula: OZn
Chemical formula: ZnO
```


## Crystallographic parameters

```
\begin{tabular}{lc}
\hline Crystal system: & Hexagonal \\
Space group: & P63mc \\
Space group number: & \multicolumn{1}{c}{186} \\
a (Å): & 3.2568 \\
b (Å): & 3.2568 \\
c (Å): & 5.2125 \\
Alpha ( \({ }^{\circ}\) ): & 90.0000 \\
Beta ( \({ }^{\circ}\) ): & 90.0000 \\
Gamma ( \({ }^{\circ}\) ): & 120.0000 \\
Calculated density (g/cm^3): & 5.64 \\
Volume of cell (10^6 pm^3): & 47.88 \\
Z: & 2.00 \\
RIR: & 5.26
\end{tabular}
```


## Status, sub files and quality

Status:
Sub files:

Quality:

Diffraction data collected at non ambient temperature
Inorganic
Alloy, metal or intermetalic
Corrosion
Modeled additional pattern
Calculated (C)

## Comments

```
ICSD collection code:
065121
```


## References

```
Primary reference: Calculated from ICSD using POWD-12++, (1997)
Structure:
```


## Peak list

| No. | $h$ | $k$ | $l$ | $d[A]$ | 2Theta[deg] | $I[\%]$ |
| ---: | ---: | ---: | ---: | :--- | :---: | ---: |
| 1 | 1 | 0 | 0 | 2.82049 | 31.699 | 57.1 |
| 2 | 0 | 0 | 2 | 2.60626 | 34.382 | 41.6 |
| 3 | 1 | 0 | 1 | 2.48062 | 36.182 | 100.0 |
| 4 | 1 | 0 | 2 | 1.91416 | 47.459 | 21.0 |
| 5 | 1 | 1 | 0 | 1.62841 | 56.463 | 29.1 |
| 6 | 1 | 0 | 3 | 1.47933 | 62.760 | 25.1 |
| 7 | 2 | 0 | 0 | 1.41024 | 66.216 | 3.8 |
| 8 | 1 | 1 | 2 | 1.38101 | 67.805 | 20.3 |
| 9 | 2 | 0 | 1 | 1.36130 | 68.924 | 10.0 |
| 10 | 0 | 0 | 4 | 1.30313 | 72.472 | 1.6 |
| 11 | 2 | 0 | 2 | 1.24031 | 76.786 | 3.0 |
| 12 | 1 | 0 | 4 | 1.18297 | 81.258 | 1.5 |
| 13 | 2 | 0 | 3 | 1.09497 | 89.415 | 5.8 |

## Stick Pattern

Intensity [\%]


## Lattice Constant For plane (100)

$$
\begin{equation*}
\frac{1}{d^{2}}=\frac{4}{3} \frac{h^{2}+h k+k^{2}}{a^{2}}+\frac{l^{2}}{c^{2}} \tag{1}
\end{equation*}
$$

For (100) plane
$\frac{1}{(2.82229)^{2}}=\frac{4}{3} \frac{1+0+0}{a^{2}}+\frac{0}{c^{2}}$
$\therefore \quad a^{2}=10.5618$
$\therefore \quad \mathrm{a}=3.2499 \mathrm{~A}^{0}$

| Lattice Constant | Standard value $\left(\mathrm{A}^{0}\right)$ | Mean calculated value $\left(\mathrm{A}^{0}\right)$ |
| :---: | :--- | :---: |
| a | 3.2568 | 3.2499 |
| b | 3.2568 | 3.2499 |
| c | 5.2125 | 5.2624 |


| $2 \theta$ <br> degree | $\Theta$ degree | $\beta$ FWHM radian |
| :---: | :---: | :---: |
| 31.6778 | 15.8389 | 0.005861 |
| 34.1601 | 17.08005 | 0.005861 |
| 36.1594 | 18.0797 | 0.010885 |
| 47.4053 | 23.70265 | 0.006699 |
| 56.4841 | 28.24205 | 0.009211 |
| 62.7602 | 31.3801 | 0.009211 |
| 66.0204 | 33.0102 | 0.008373 |
| 67.6551 | 33.82755 | 0.005861 |
| 68.9021 | 34.45105 | 0.010048 |
| 72.378 | 36.189 | 0.013397 |
| 76.7111 | 38.35555 | 0.010048 |



1 radian $=\pi / 180=0.01745$ 1 degree $=57.25$ radian

Crystallite size (D) using Scherrer's formula :

$$
\begin{aligned}
D & =\frac{0.9 \lambda}{\beta \cos \theta} \\
& =\frac{0.9 \times 0.154}{0.005861 \times \cos (0.2763)} \\
& =\frac{1.386}{0.9620 \times 0.005861} \\
D & =24.5883 \mathrm{~nm}
\end{aligned}
$$

Similarly remaining values of ' $D$ ' can be calculated by using above formula.

Average of crystallite size $D$ in $n m=\mathbf{2 6 . 7 3} \mathbf{n m}$

Crystallite Size ' $D$ ' in nm
24.5883
24.7460
13.3985
22.6035
17.0855
17.6297
19.7428
28.4705
16.7306
12.8203
17.5923

NRF : Nelson - Riley Function

$$
\begin{aligned}
N R F & =\frac{1}{2}\left(\frac{\cos ^{2} \theta}{\sin \theta}+\frac{\cos ^{2} \theta}{\theta}\right) \\
& =\frac{1}{2}\left(\frac{\cos ^{2}(0.2263)}{\sin (0.2263)}+\frac{\cos ^{2}(0.2263)}{0.2263}\right) \\
& =\frac{1}{2}\left(\frac{0.9225}{0.2727}+\frac{0.9985}{0.2309}\right) \\
& =\frac{1}{2}[3.381908+3.339043] \\
N R F & =3.3714
\end{aligned}
$$



| (h k I) <br> plane | NRF | a ( $\mathrm{A}^{0}$ ) |
| :---: | :---: | :---: |
| (100) | 3.3714 | 3.2499 |
| (002) | 3.0899 |  |
| (101) | 2.889 | 3.2505 |
| $\left(\begin{array}{lll}1 & 2\end{array}\right)$ | 2.0575 | 3.2287 |
| (110) | 1.6084 | 3.2556 |
| (103) | 1.3663 | 3.1784 |
| (200) | 1.2567 | 3.2652 |
| (112) | 1.2052 | 3.2536 |
| (201) | 1.1674 | 3.2553 |
| $\left(\begin{array}{ll}0 & 4\end{array}\right)$ | 1.0682 |  |
| $\left(\begin{array}{ll}2 & 2\end{array}\right)$ | 0.9557 | 3.2511 |

Strain

| $\operatorname{Sin} \Theta / \lambda$ | $\beta \cos \Theta / \lambda$ |
| :--- | :--- |
| 0.1770 | 0.00366 |
| 0.1905 | 0.003637 |
| 0.2013 | 0.006717 |
| 0.2608 | 0.00398 |
| 0.3070 | 0.005268 |
| 0.3378 | 0.005105 |
| 0.3534 | 0.004559 |
| 0.3611 | 0.003161 |
| 0.3670 | 0.005379 |
| 0.3830 | 0.00702 |
| 0.4026 | 0.005116 |

D = 1/intercept =1/0.00369
$D=271.0071 \mathrm{~A}^{\circ}$
$D=27.1007 \mathrm{~nm}$
Slope $(\varepsilon)=0.00388$

$$
\begin{gathered}
\beta=\frac{\lambda}{D \cos \theta}-\varepsilon \tan \theta \\
\beta=\frac{\lambda}{D \cos \theta}-\varepsilon \frac{\sin \theta}{\cos \theta} \\
\beta \cos \theta=\frac{\lambda}{D}-\varepsilon \sin \theta \\
\left(\begin{array}{rl}
\beta \cos \theta \\
\lambda & )
\end{array}\right. \\
y=c-m x \\
y \\
y=m x+c
\end{gathered}
$$



## Texture Coefficient:

$$
\begin{aligned}
T C & =\frac{I_{(h k l)} / I O_{(h k l)}}{\frac{1}{N} \sum\left[I_{(h k l)} / I O_{(h k l)}\right]} \\
& =\frac{66.09 / 57.1}{\frac{1}{11}[12.60108]} \\
& =1.010379
\end{aligned}
$$

The reflection intensities from XRD pattern contain information related to the preferential or random growth of polycrystalline thin films which is studied by calculating the texture coefficient $\mathrm{TC}(\mathrm{hkl})$. TC for the ( $\left.\begin{array}{lll}0 & 0 & 2\end{array}\right)$ plane has relatively higher value than (100) and (200) plane. This result conforms that the c-axis crystal orientation of ZnO .

| ( hk I ) plane | Texture coefficient |
| :---: | :---: |
| $\left(\begin{array}{lll}1 & 0\end{array}\right)$ | 1.010379 |
| (002) | 1.198195 |
| (101) | 0.872941 |
| $\left(\begin{array}{lll}1 & 2\end{array}\right)$ | 0.846753 |
| (110) | 0.929637 |
| $\left(\begin{array}{ll}1 & 3\end{array}\right)$ | 0.792255 |
| (200) | 1.196848 |
| (112) | 1.0686 |
| (201) | 1.086811 |
| (004) | 0.938412 |
| $\left(\begin{array}{ll}2 & 2\end{array}\right)$ | 1.059168 |

## Standard Deviation

$$
\begin{aligned}
& \sigma=\frac{\sqrt{\sum \mathrm{I}_{(\mathrm{hkl})}^{2}-\left(\sum \mathrm{I}_{(\mathrm{hkl})}\right)^{2} / \mathrm{N}}}{\mathrm{~N}} \\
& \sigma=\sqrt{\frac{20338.42-(345.2 / 11)}{11}} \\
& \sigma=29.39607
\end{aligned}
$$

